Numerical simulation of the dynamic compression of a 6061-T6 aluminum metallic foam

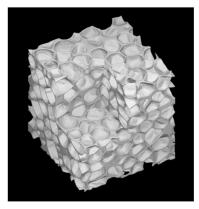
Biswajit Banerjee and Anup Bhawalkar

Center for the Simulation of Accidental Fires and Explosions University of Utah

7th World Conference on Computational Mechanics, 2006

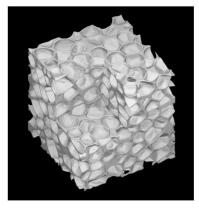
Outline

- Motivation
 - Previous Work
- 2 Approach
- The Plasticity Model
- Creation of Foam Microstructures
- 6 Crushing of Foam Microstructures



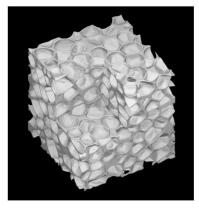
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- High weight to specific mechanical stiffness.
- Used for:
 - High-capacity impact absorption.
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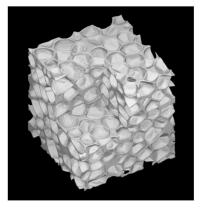
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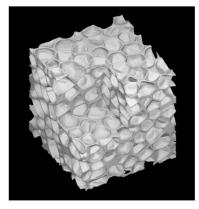
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- Determination of dynamic structure/property relations.
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- Parallel multiphysics framework.
- Large deformation solid mechanics with the Material Point Method (MPM).

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- Fluid-structure interaction on a common grid. (Kashiwa et al., 2000;
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The Process

- Determination of parameters for the Mechanical Threshold Stress model for 6061-T6 aluminum.
- Creation of foam microstructures by pressurization of bubbles of soft material.
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$$\sigma_{V}(\epsilon_{p}, \dot{\epsilon}, T, p) = (\sigma_{a} + S_{i}\sigma_{i} + S_{e}\sigma_{e}) \frac{\mu(T, p)}{\mu_{0}}$$
 (1)

- The athermal part contains the effect of grain size.
- The scaling factors depend on strain-rate, temperature, and pressure.
- Uses an empirical strain hardening model (modified Voce model)

$$\frac{d\sigma_{\theta}}{d\epsilon_{D}} = \theta_{0}(T) \left[1 - f(\sigma_{\theta}) \right] \tag{2}$$

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Shear Modulus Model

 We use a temperature and pressure dependent shear modulus model (Nadal and Le Poac, 2003; Guinan and Steinberg, 1974)

$$\mu(T, p) = \frac{1}{\mathcal{J}(T/T_m)} \left[\left(\mu_0 + \frac{\partial \mu}{\partial p} \frac{p}{\eta^{1/3}} \right) \left(1 - \frac{T}{T_m} \right) + \frac{\rho}{Cm} k_b T \right]$$
(3)

 We use a pressure dependent melting temperature model (Burakovsky et al., 2000)

$$T_m(p) = T_m(0) \left[\frac{1}{\zeta} + \frac{1}{\zeta^{4/3}} \frac{\mu'_0}{\mu_0} p \right]$$
 (4)

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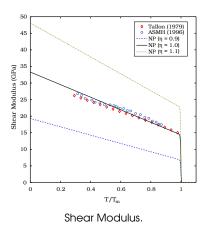
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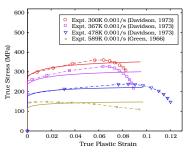
Model Validation: Shear and Melt Models



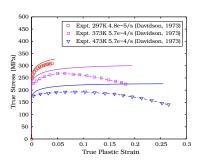
6000 Boehler and Ross (1997) Burakovsky et al. (2000) BPS Melt Model 4000 2000 50 -50 0 100 150 Pressure (GPa)

Melt Temperature.

Model Validation: Flow Stress Model

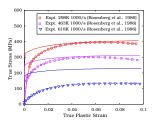


Strain rate = 0.0001/s.

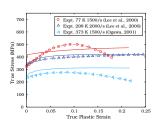


Strain rate = 0.0057/s.

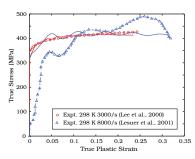
Model Validation: Flow Stress Model



Strain rate = 1000/s.

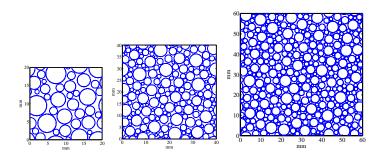


Strain rate = 1500-2000/s.



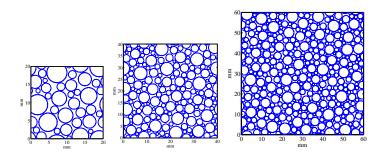
Strain rate = 3000-8000/s.

Bubble Creation



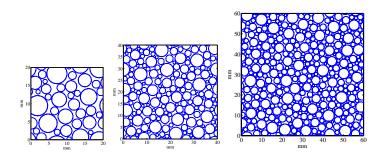
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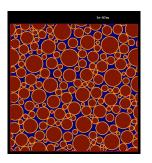


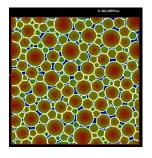
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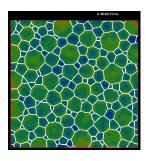
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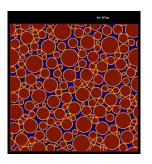
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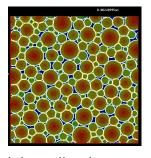


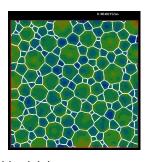




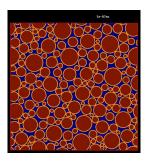
- Use fluid-structure interaction to expand bubbles.
- Compressible Neo-Hookean solid with K=0.6 MPa and $\mu=0.3$ MPa.
- Gas inside bubbles is pressurized by adding heat.
- Gas between bubbles has low pressure and temperature.

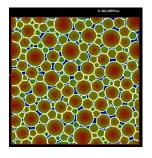


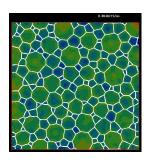




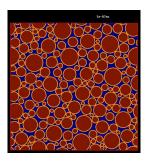
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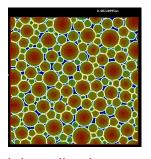






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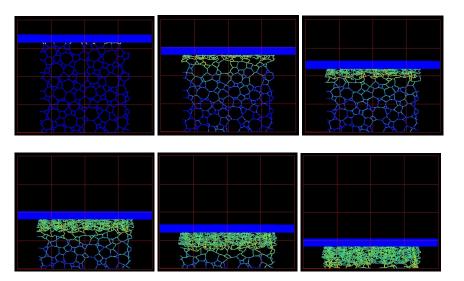




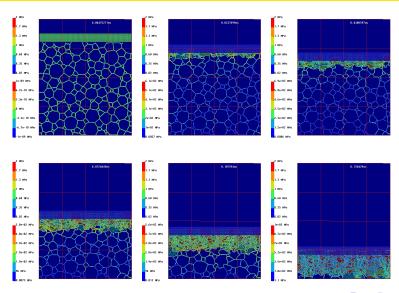


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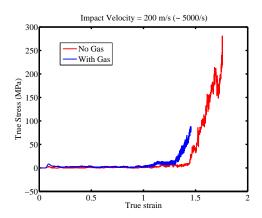
Crushing Without Interior Gas



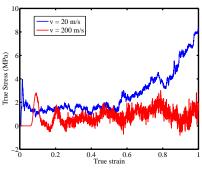
Crushing With Interior Gas



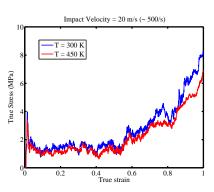
Stress-Strain Curves



Effect of Strain-Rate and Temperature



Effect of Strain Rate

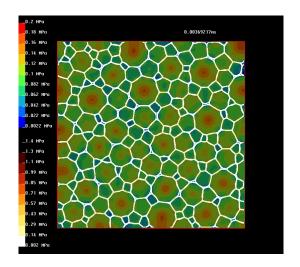


Effect of Temperature

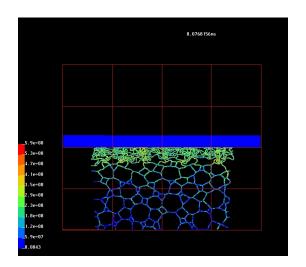
Summary

- MTS plasticity model of 6061-T6 Al.
- A novel way of creating a foam microstructure.
- There is a clear effect of including gas in the stress-strain curves.
- Crushing of foam shows no shear banding.
- Further work is needed to create a macroscopic model of the dynamic response of Al foam.

Creation of Foam Microstructure



Crushing of Empty Foam



Crushing of Gas-Filled Foam

